Seismic Risk Mitigation Studies: The Portuguese Experience.

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European Council of Civil Engineers





Seismic Risk Mitigation Studies. The Portuguese Experience

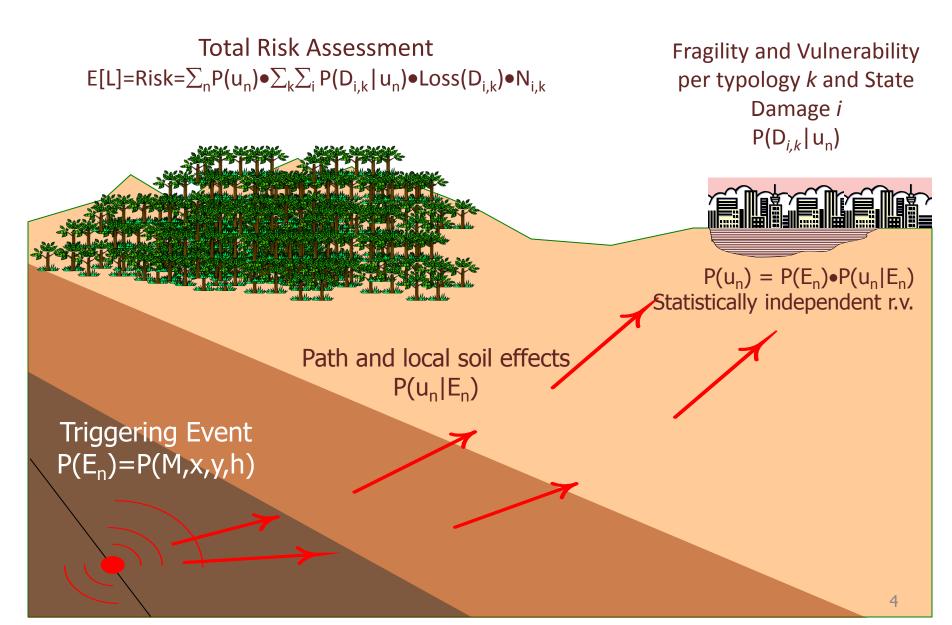
Summary

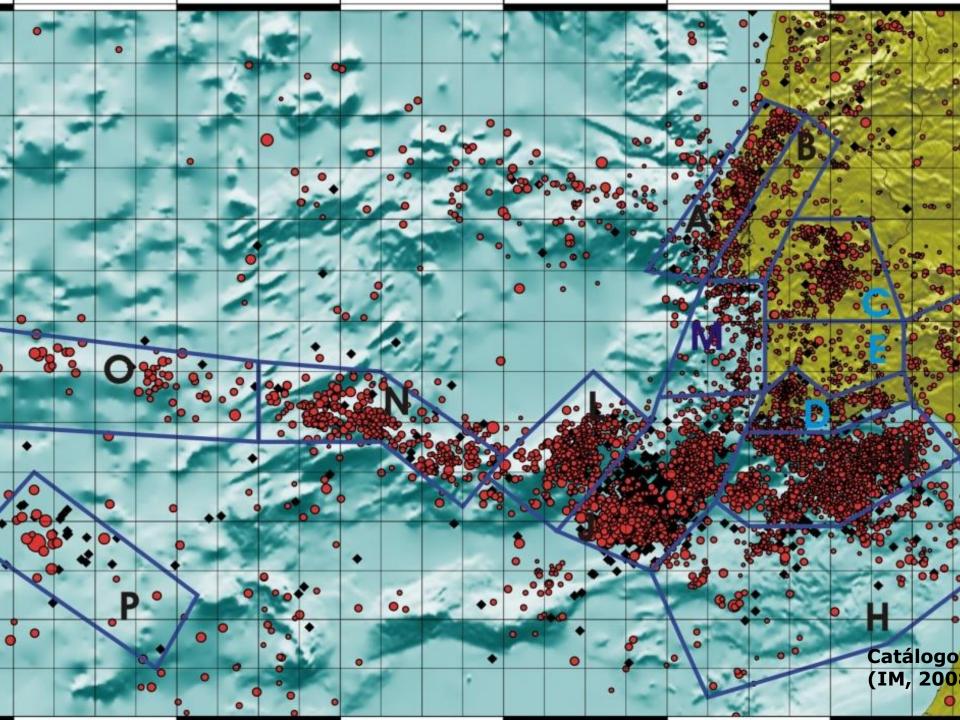
- Overview on Seismic Risk and Mitigation Strategies Analysis SRMA
- 2. LNECloss a tool for seismic loss estimation ANPC (MAL and ERSTA) ; LESSloss ... GEM₁
- 3. The case study of the Metropolitan Area of Lisbon (MAL)
- 4. Conclusions regarding the case study
- Experimental research in seismic strengthening of buildings in Portugal.

Seismic Risk and Mitigation Analysis (SRMA)

- <u>Seismic Risk and Mitigation Analysis</u> (SRMA) \Rightarrow Methodology based on Probabilistic <u>Seismic Risk Analysis</u> taken with <u>Mitigation Strategies</u> based on structural earthquake engineering to support the decision to reduce SR.
- <u>Mitigate SR</u> \Rightarrow Consistent methods to reduce the effects of earthquakes on population, on civil engineering structures and on infra-structures taking into account <u>uncertainties</u> (epistemic and natural)
- SRMA are Interdisciplinary of studies ⇒ interaction of different specialized sub-fields of research;
 - Engineering seismology.
 - Earthquake engineering.
 - Probability seismic risk analysis.
 - Cost benefit analysis.

Probabilistic Seismic Risk Analysis





Process of Seismic Hazard Disaggregation

- Seismic Hazard Analysis (PSHA) for given site
 - SHA To compute the probability of a given intensity level of being exceed in a given time interval (generally one year) based on probabilistic methods.
 - Source energy Events occur at random in *space*, *time* and *magnitude*
 - Attenuation process For a given event, site intensities are also *random processes*.

$$P(U > u)_{k} = \iint_{R}^{mu_{k}} P(U > u \mid m, R) \cdot f_{M}(m)_{k} \cdot f_{R}(R)_{k} \cdot dm \cdot dR$$

$$\omega_{k} = v_{k} \cdot P(U > u)_{k} \quad \text{Annual mean rate of occurrence of } u$$

$$P(U > u) = 1 - e^{\left(-\sum_{k=1}^{n} \omega_{k}\right)} \quad n \text{ independent Poisson processes}$$

$$RP(U > u) = \frac{1}{1 - e^{\left(-\sum_{k=1}^{n} \omega_{k}\right)}} \quad \text{Return Period}$$

Process of Seismic Hazard Disaggregation

- Seismic Hazard Disaggregation
 - Which are the modal value (or values) of the of the *pdf* corresponding to the *CDF:* $P(U \le u) = 1 P(U > u)$.
 - Likelihood function of the of independent variables *m,x,y* given an event *U* > *u_i*. occurred in site.

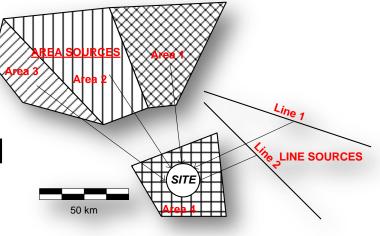
$$\ell(m, x, y | U > u_i) = \sum_{k}^{n} f_S(x, y) \cdot f_M(m)_k \cdot P(U > u_i / m, R_i)_k$$

 $f_S(x, y)$ spatial distribution of the relative the frequency of events in all seismic zones

• The values for which *m*, *x* and *y* gives maximum defines the modal event.

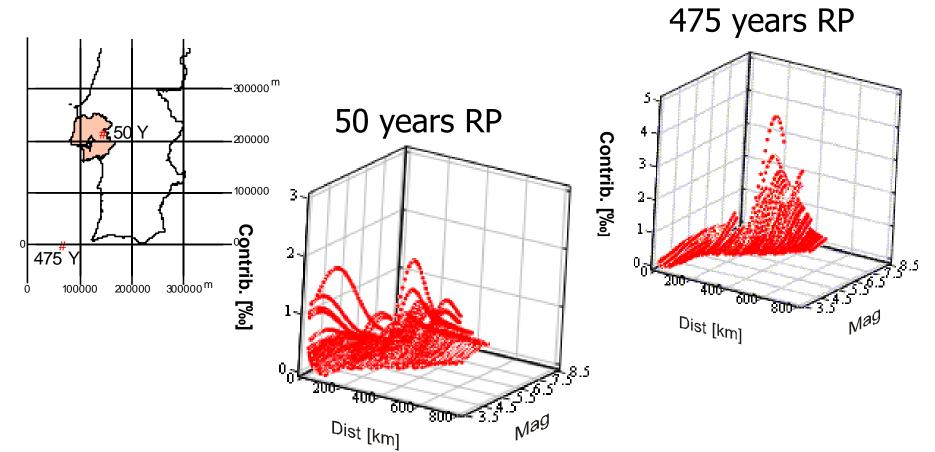
$$\widetilde{E}_{i} = \left\langle \widetilde{m}_{i}, \widetilde{x}_{i}, \widetilde{y}_{i} \middle| U > u_{i} \right\rangle = max[\ell(m, x, y \middle| U > u_{i})]$$

• For each return period it is possible to define a modal event



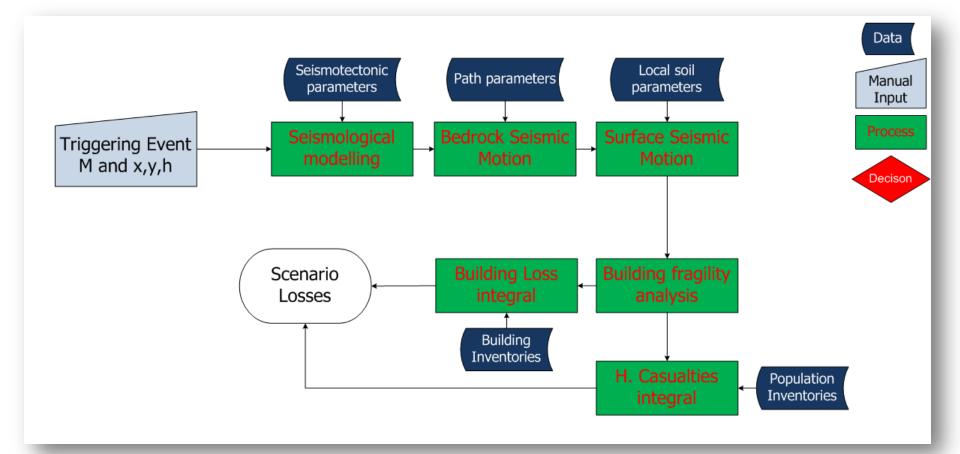
Seismic input definition

• Earthquake scenario based on PSHA disaggregation



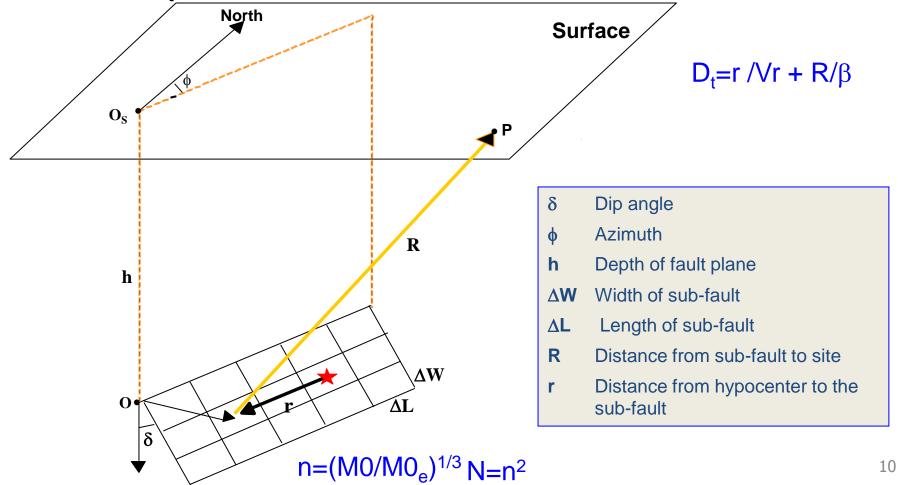
LNECloss - Seismic Loss Scenario Simulator

• Seismic loss assessment for a deterministic scenario



LNECloss - Seismic Scenario simulator Bedrock seismic motion

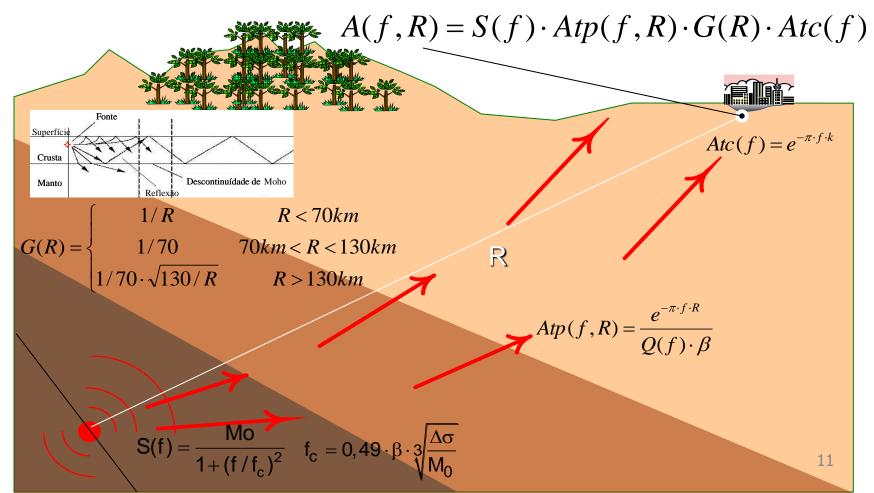
Finite fault modeling: Fault plane divided in sub-faults considered point sources. Contributions synthesized at the local site taking into account delay time D_t rupture velocity and focal distance.



LNECloss – Seismic Scenario simulator

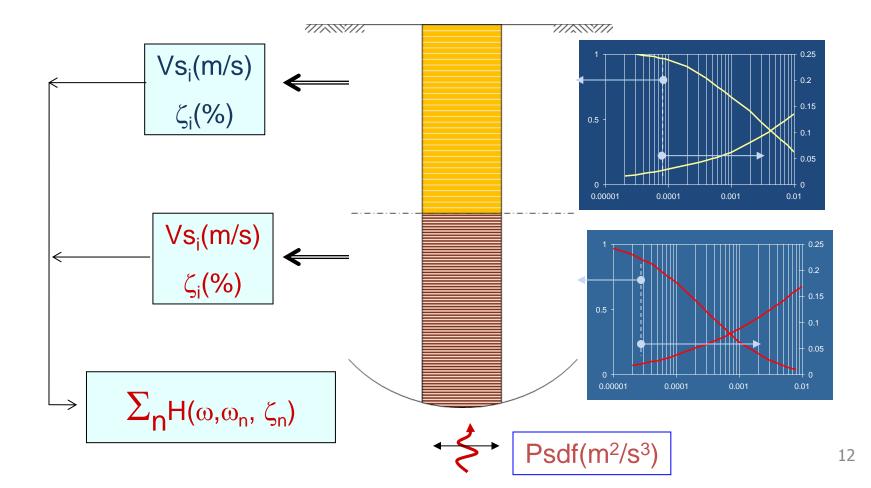
Seismological modelling module

Seismological model for synthetic motions at bedrock level; Boore (1983; 2003) – point source Gail Atkinson et. al. (1998; 2002) – finite fault model source A. Carvalho (2006) – stochastic finite fault model source



LNECloss - Seismic Scenario simulator Modelling of soil site effects

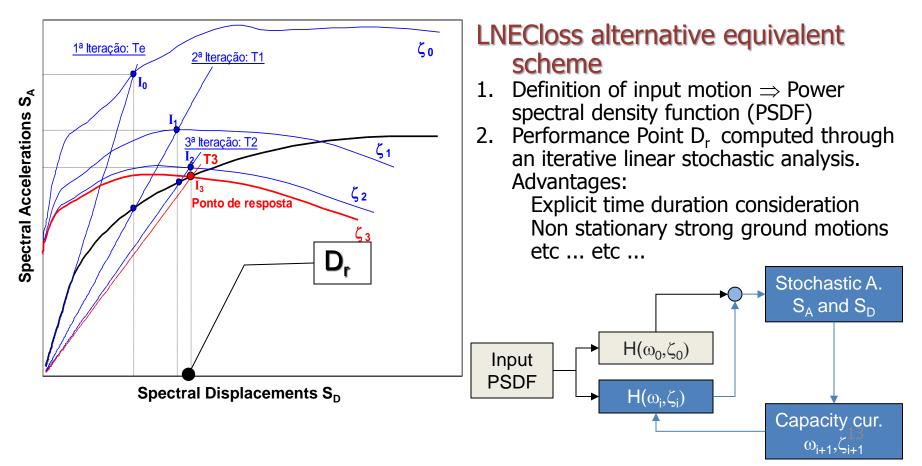
Motions at surface by inelastic modelling of site soil conditions SHAKE – Deterministic analisys in frequency domain Bilé Serra (1998) – Stochastic analysis



LNECloss - Seismic Scenario simulator <u>Fragility analysis of building typologies</u>

FEMA & NIBS methodology (HAZUS99) - Vulnerability

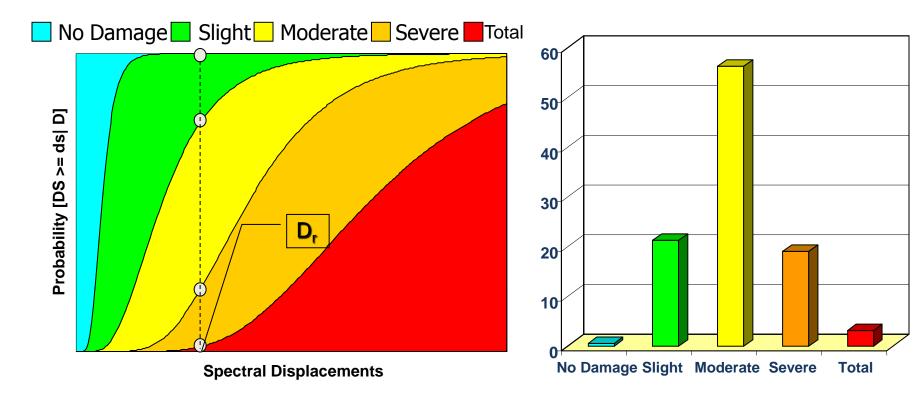
1. Evaluation of building responses through a <u>capacity curve</u> non linear FxD \Rightarrow S_AxS_D Displacement Based Assessment - Response Spectra (Er) & iterative computation of the \Rightarrow Performance Point D_r



LNECloss - Seismic Scenario simulator <u>Fragility analysis of building typologies</u>

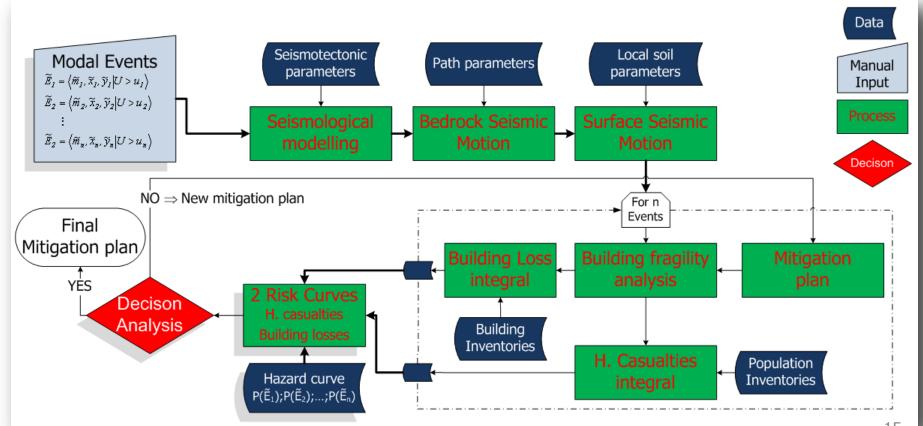
FEMA & NIBS Methodology (HAZUS99 software) – FRAGILITY

- 1. Introduction of the Limit Damage States
- 2. Fragility defined in terms of structural response and not seismic intensity



LNECloss - Seismic Scenario simulator

• Probabilistic Seismic Risk Analysis based on modal events

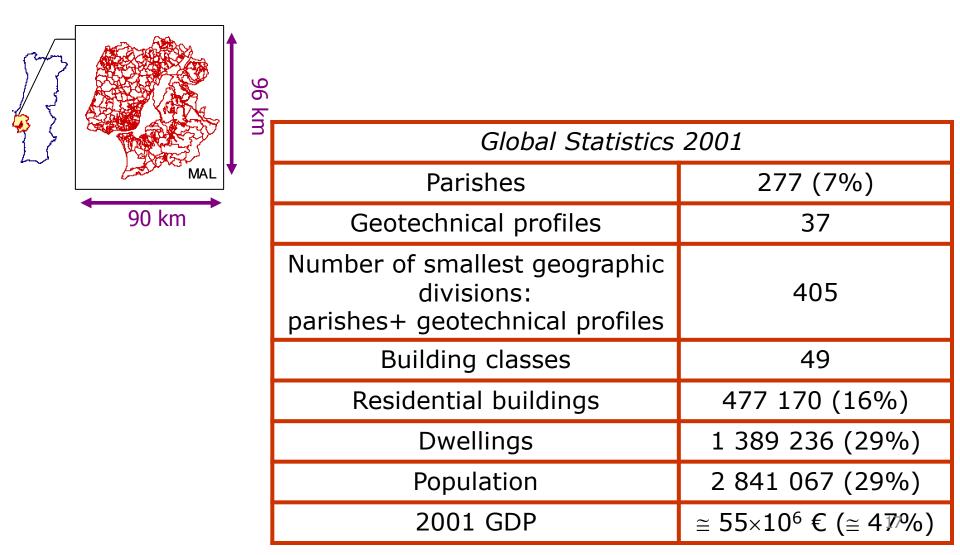


Choice of case study area Metropolitan Area of Lisbon - MAL



3 x 10⁶ inhabitants

Case study area: Metropolitan Area of Lisbon - MAL



Case study area: Metropolitan Area of Lisbon - MAL

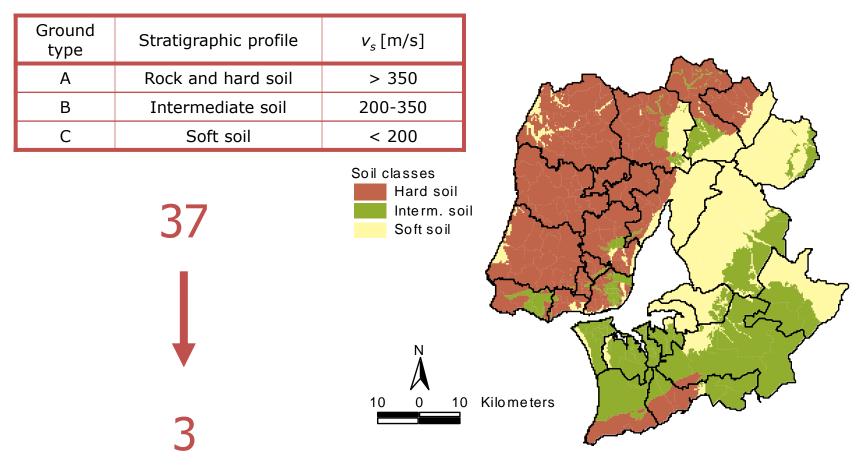


- Vulnerability and inventory definition
- Soil classification

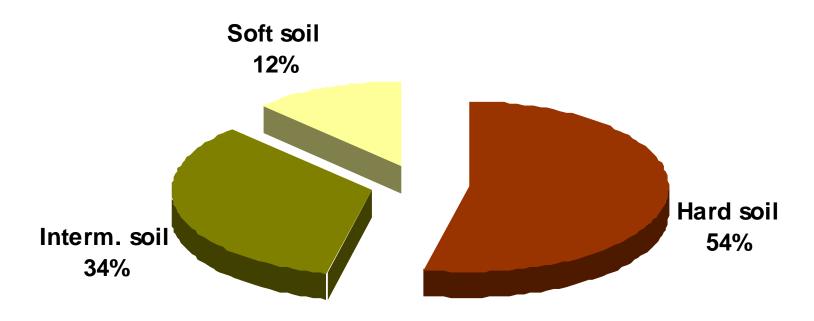
37 soil profiles



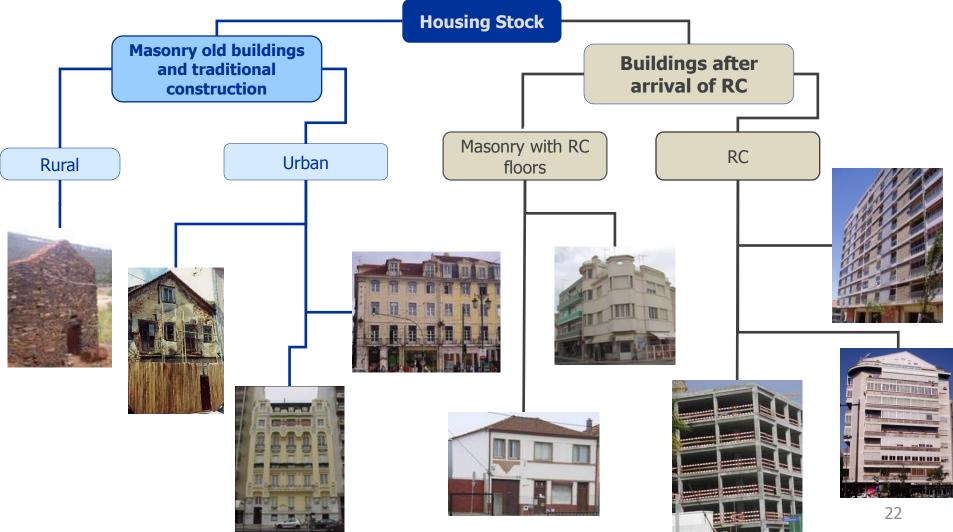
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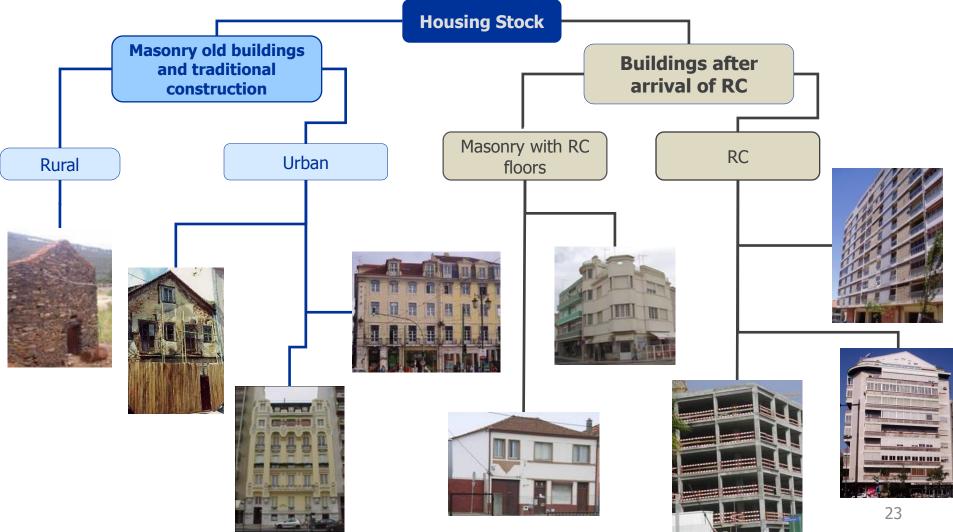
- Vulnerability and inventory definition
- Exposure analysis by soil classification
- Economic values Repair and replacement cost of the MAL residential building stock ≈ 134 000 10⁶€ (based on official replacement cost/m²)



- Vulnerability and inventory definition
- Characterization of MAL housing stock



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- Characterization of MAL housing stock



Vulnerability and inventory definition

• 7 vulnerability classes x 7 n^o floors

LNECloss 49

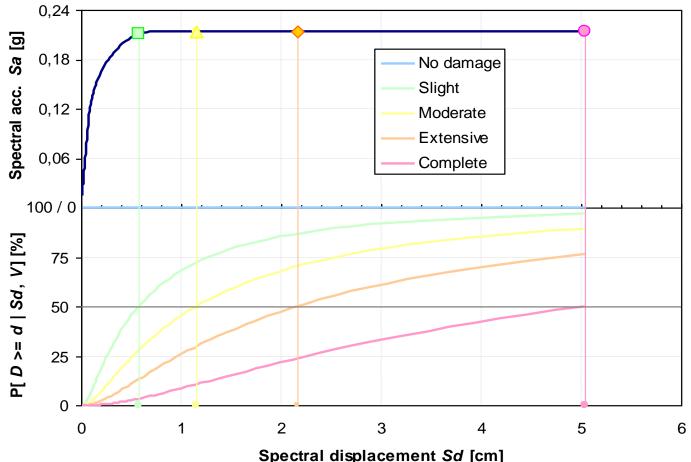
CENSOS 315

Seismic Vulnerability classes Adobe + rubble stone + others Masonry before 1960 Masonry 1961-85 Masonry 1986-01 RC before 1960 RC 1961-85 RC 1986-01

Vulnerability and inventory definition

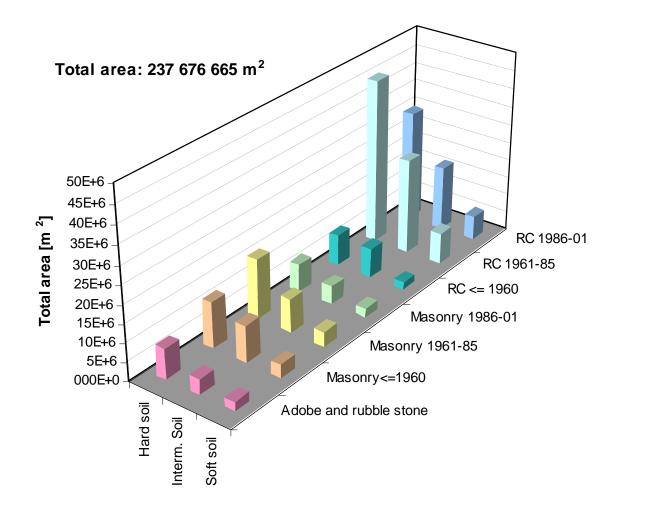
• Capacity curves fragility distributions

Capacity curves fragility distributions where adopted for 49 Typologies

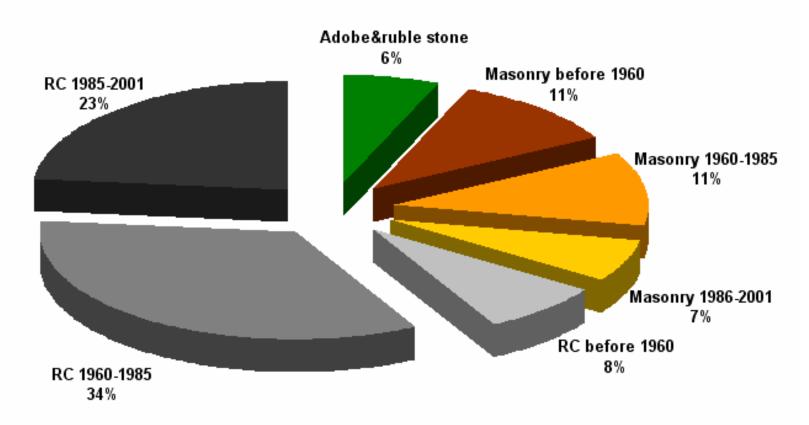


Vulnerability and inventory definition

• Exposure analysis

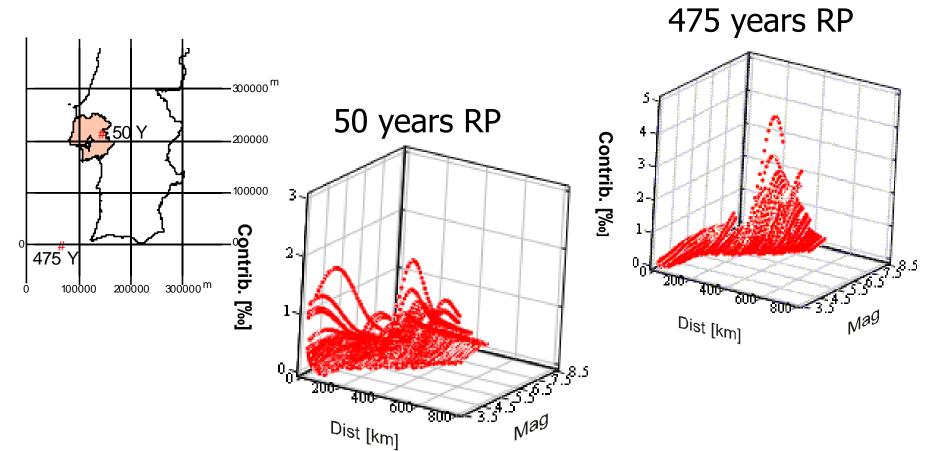


- Vulnerability and inventory definition
- Exposure analysis
- Economic values Repair and replacement cost of the MAL residential building stock \approx 134 000⁻¹⁰⁶ (based on official replacement cost/m²)



Seismic input definition

• Earthquake scenario based on PSHA disaggregation



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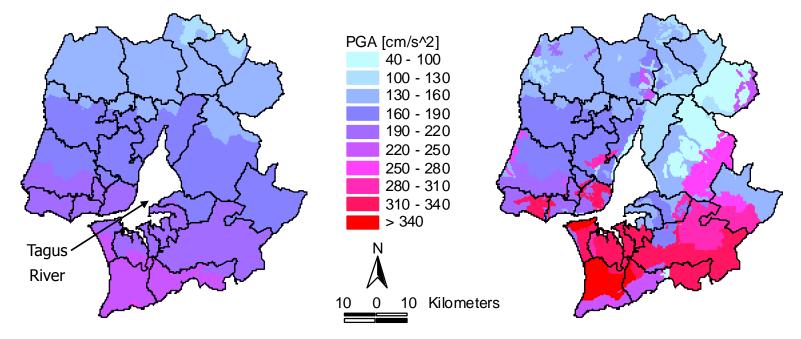
Return	Loca	ation	Magnitude		
Period	X [Km]	Y [Km]	М		
95	67.3	-4.4	7.2		
200	67.3	-4.4	7.6		
475	67.3	-4.4	7.9		
700	67.3	-4.4	8.1		
975	67.3	-4.4	8.2		
2000	67.3	-4.4	8.4		
5000	67.3	-4.4	8.5		

Case Study of Probabilistic Risk Analysis

Shake Maps Scenarios

• Modelling earthquake scenario

475 years RP scenario



PGA for bedrock

PGA considering soil amplification

Loss estimation

Loss estimates for actual region

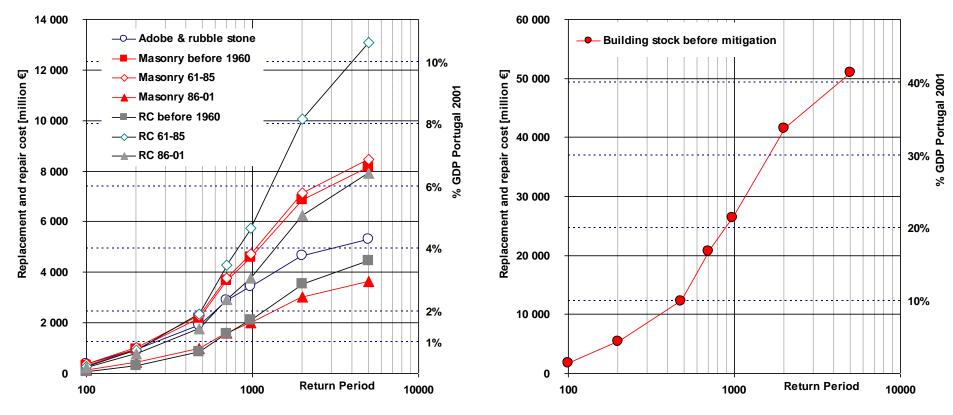
$$E(L/u) = Ne_T \cdot \sum_d \sum_v A_v \cdot DR_d \cdot P_D(D = d/u) \cdot P_V(V = v)$$

 Ne_{T} - total number of buildings in the studied region

 A_v - is the average floor area of with vulnerability v $P_D(D = d | u)$ - is the damage probability matrix $P_V(V = v)$ – existing relative frequency of vtypological class in the studied region DR_d – Damage ratio which defines the % of loss of a building that are in damage state d E(L|u) x replacement cost/m² = Loss in terms of replacement cost

Damage state	Damage Ratio, DR _d [%]			
Slight	2			
Moderate	10			
Severe	50 100			
Complete				

• Loss estimates for region without mitigation



Most of the loss comes from:

- 1. Non ductile RC buildings constructed between 1961-1985
- 2. Masonry buildings constructed between 1961-1985 and before 1960

32

60%

Loss estimates for modified city

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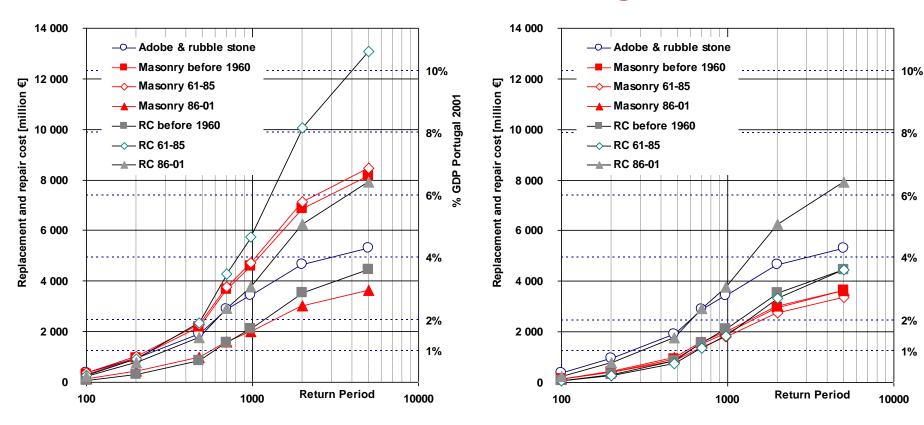
Modeling strengthening interventions – Selective interventions

(R. Pinho, 1998)

# Streng	ason ry	RC -	Improvement of force capacity		Improvement of ductile capacity.						
	Ž	H	λ	γ	δ_d		□ slight	♦ moderate	△ extensive	o complete	
1	\checkmark	\checkmark	-	25%	250/	306% 2	*	Δ		0	
2	\checkmark	√	-	50%	25%	ຍັ _ຍ 200%					
3	\checkmark	√	-	75%	25%	ື່ສູ ຮັ້ງ 175%					
4	\checkmark	\checkmark	75%	75%	25%	150% 125%					
5	\checkmark	\checkmark	-	25%	50%	Sa Reinfor			0		
6	\checkmark	√	-	50%	50%	Sa	1				
7	\checkmark	√	-	75%	50%		ľ		I		
8	\checkmark	√	75%	75%	50%		0	3 Spectr	6 al displacemer	9 9	12
9		\checkmark	-	25%	75%			Opeen			
10		\checkmark	-	50%	75%	•					
11		\checkmark	-	75%	75%	-					2.4
12		\checkmark	75%	75%	75%	-					34

Loss estimates for modified city

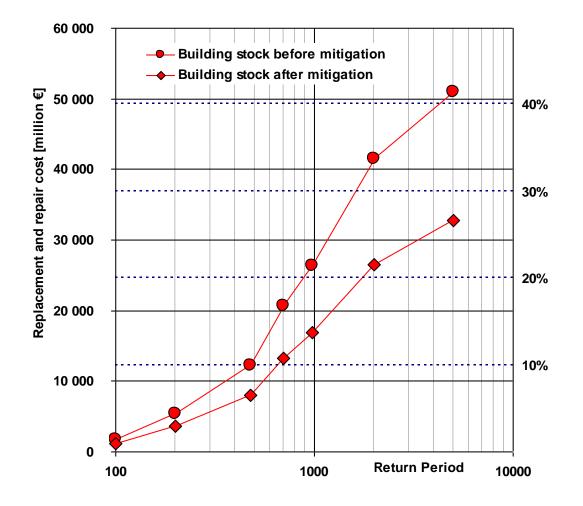
Building Stock Before Str.



Building Stock After Str.

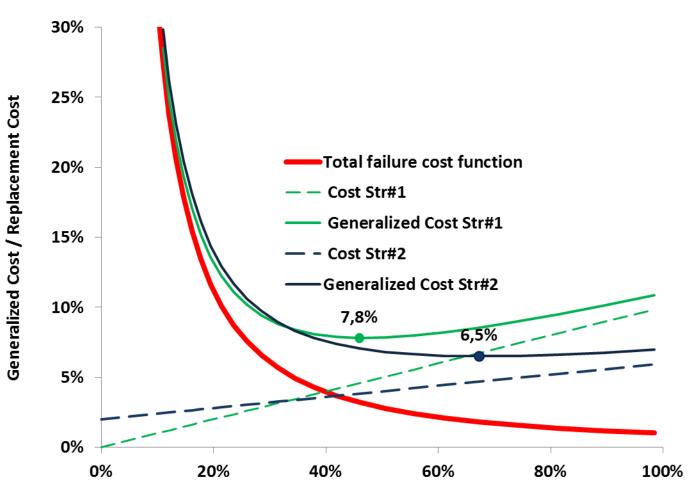
% GDP Portugal 2001

Loss estimates for modified city



Seismic Risk Assessment and Mitigation Strategies

Generalized Cost-Benefit Analysis (*Ferry Borges*) *Generalized Cost* – Strengthening Cost + Total failure costs *Benefits* – Risk Mitigation + Resilience Increase



Strengthening Level / Initial Strength

Conclusions

Economic seismic risk of the Metropolitan Area of Lisbon (MAL), in terms of replacement cost induced to the residential building stock was assessed. It was found that values varying from <u>1.3%</u>, for 95 years return period, up to <u>38%</u>, for 5000 years return period, of the total replacement cost of MAL residential stock buildings.

After the implementation of a given strengthening strategy, based on selective retrofitting interventions and applied to typological building classes responsible for the larger amount of the economic seismic risk (60%), it was concluded that economic risk could be mitigated by an amount of 36% for all return periods.

The mitigation of masonry buildings results in higher absolute benefits then mitigation strategies applied to RC structures, mainly when human casualties are considered. When mitigation is analyzed in relative terms, regarding to the reference situation, the selective retrofitting interventions applied to RC structures result in higher benefits.

The maps of loss estimation after the implementation of the purposed mitigation actions show that the chosen mitigation action has predominant effects on the South margin of Tagus River, where intermediate soils prevail.

Improvements of ductile capacity play a more important role in mitigation benefits than force capacity improvement does.

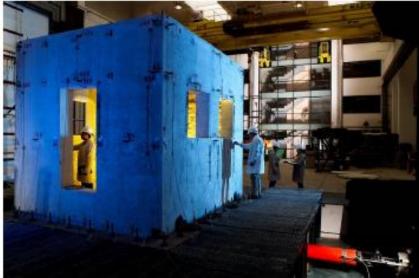
Maybe explained by methodology adopted to define damage states which are exclusively based on displacement demands and capacities.

In the absence of a criterion to select the optimal intervention, like a costbenefit analysis, upper bounds interventions, both in RC as in masonry buildings intervened, correspond to the highest benefits.

Experimental research on seismic strengthening of buildings in Portugal.

Experimental research in seismic strengthening of buildings in Portugal.







Thanks for your attention alf@Inec.pt